

FAQs

1. Give the moment coefficients for bending moment calculations as per IS 456:2000

Type of load	Span Moments		Support Moments	
	Near the middle of end span	At middle of interior span	At support next to the end support	At other interior supports
Dead load and imposed load (fixed)	+1/12	+1/16	- 1/10	- 1/12
Imposed load (not fixed)	+1/10	+1/12	- 1/9	- 1/9
For obtaining BM, the coefficient shall be multiplied by the total design load and effective span				

2. Design a three span one way continuous roof slab for a residential building of effective span 3m. It carries a live load of 1.5 kN/m² and weathering course and tile of 1.0 kN/m². Adopt M20 concrete & Fe415 steel. Draw the reinforcement details also.

a. Load calculations:

- i. Dead loads:

Assuming thickness of slab from Cl. 23.2.1

$$\begin{aligned}
 l/d &= 26 \\
 d &= 3000/26 = 115.40 \\
 D &= 115.40 + 15 + 8/2 = 134.38\text{mm} \\
 \text{Assume } D &= 125\text{mm} \\
 \text{Self weight of slab} &= 0.125 \times 25 = 3.125 \text{ kN/m}^2 \\
 \text{Weight of weathering course and tiles} &= 0.025 \times 24 = 1.0 \text{ kN/m}^2 \\
 \text{Total dead loads } w_d &= 4.125 \text{ kN/m}^2 \\
 \text{ii. Live load on slab } w_l &= 3.0 \text{ kN/m}^2
 \end{aligned}$$

b. Moment calculations:

i. Span moments

$$\text{Moment near the middle of end span} = w_d l^2 / 12 + w_l l^2 / 10 = 5.79 \text{ kNm}$$

$$\text{Moment at the middle of interior span} = w_d l^2 / 10 + w_l l^2 / 12 = 4.57 \text{ kNm}$$

ii. Support moments

$$\text{Moment at support next to end support} = -w_d l^2 / 10 - w_l l^2 / 9 = -6.71 \text{ kNm}$$

$$\text{Moment at other interior supports} = -w_d l^2 / 12 - w_l l^2 / 9 = -6.09 \text{ kNm}$$

c. Effective depth of slab:

here maximum BM $M_d = 6.71 \text{ kNm}$

$$M_u = 1.5 \times 6.71 = 10.065 \text{ kNm}$$

by equating M_u to $M_{u,lim}$,

$$d = 60.39 \text{ mm} < 106 \text{ mm}$$

Hence safe against moment.

Hence keep $D = 125 \text{ mm}$; $d = 106 \text{ mm}$

d. Area of reinforcement – Main Steel

A_{st} for Maximum bending moment

$$M_u = 0.87 f_y A_{st} (d - 0.416 x_u)$$

$$\text{where } x_u = 0.87 f_y A_{st} / 0.36 f_{ck} b$$

$$= 0.05 A_{st}$$

$$\text{Now } A_{st \text{ reg}} = 278.13 \text{ mm}^2$$

Check for Minimum steel as per IS 456:2000

$$A_{st} = 0.12\% \text{ cross sectional area}$$

$$= 127.2 \text{ mm}^2 < 278.13 \text{ mm}^2$$

$$\text{Hence } A_{st \text{ reg}} = 278.13 \text{ mm}^2$$

Provide 8mm diameter bar

$$\text{Spacing} = 180.73 \text{ mm}$$

Provide 8mm diameter bar at 160mm c/c

$$A_{st \text{ pro}} = 314.16 \text{ mm}^2$$

Distribution Steel

$$A_{st} = 0.15\% \text{ cross sectional area}$$

$$= 159 \text{ mm}^2$$

Use 6mm dia ms bar

$$\text{Spacing} = 177.83 \text{ mm}$$

Provide 6mm dia MS bar at 150mm c/c

e. Check for deflection

As per cl.23.2.1 of IS 456:2000

$$l/d = 26 \times M.F$$

$$p_t = 0.30\%$$

$$f_s = 0.58 f_y A_{st \text{ reg}} / A_{st \text{ pro}} = 213.09 \text{ N/mm}^2$$

$$\text{As per Fig.4 of IS 456: 2000; } M.F = 1.6$$

$$\text{Hence } d = 72.12 \text{ mm} < 106 \text{ mm}$$

Hence safe against deflection.